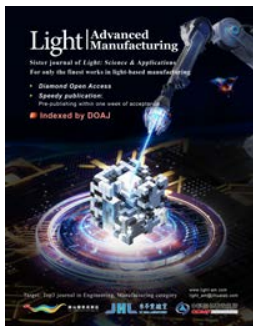


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1 **Early Detection of Lithium Battery Leakage Using a** 2 **Highly Sensitive in situ ZIF-8 Membrane-coated** 3 **Micro-nano Optical Fibre**

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21 **Abstract**

22 Detecting electrolyte leakage is an effective early warning approach for abnormal faults in
23 lithium-ion batteries (LIB) and can help mitigate safety risks such as fires and explosions. However,
24 detecting electrolyte leakage in the early stages of LIB faults presents a significant challenge, as
25 leaks in LIBs produce volatile organic compounds (VOCs) at parts per million levels that are
26 difficult to detect using conventional VOC sensors. Here, an effective LIB VOC sensor using
27 micro-nano optical fibres (MNFs) has been developed for the first time, coated with an in situ

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28 self-assembled zeolitic imidazolate framework-8 (ZIF-8) membrane as an electrolyte-sensitive layer.
29 The abundance of pores in ZIF-8 is excellent for adsorbing a variety of VOCs, including diethyl
30 carbonate, ethyl methyl carbonate, dimethyl carbonate, and propylene carbonate. The MNFs
31 possess high refractive index sensitivity, enhancing the online monitoring of electrolytes. MNFs
32 with a diameter of approximately 7 μm were assembled with four-cycle ZIF-8 of approximately 500
33 nm thickness, as the fabricated sensor. Through wavelength demodulation, the LIB sensor
34 demonstrated high sensitivity, detecting 43.6 pm/ppm of VOCs and exhibiting rapid response and
35 recovery times of typically within 10 min and 23 s, respectively, as well as a low theoretical
36 detection limit of 2.65 ppm for dimethyl carbonate vapor with excellent reversibility. The first
37 on-site verification of online LIB leakage monitoring demonstrated that the sensor achieved a 35 h
38 early warning prior to full-load leakage, thus exhibiting promising prospects for applications in
39 scenarios such as car batteries.

40 **Keywords:** Lithium battery; Electrolyte leakage; Micro-nano optical fibres; Volatile organic
41 compounds; Zeolitic imidazolate framework-8; Dimethyl carbonate

42 **Introduction**

43 Lithium-ion batteries (LIB) have attracted considerable attention as a new energy technology and
44 have been widely used in energy storage systems, dominating the portable electronic products and
45 electric vehicles markets¹⁻³. However, in most applications, external factors such as pressure,
46 vibration, temperature, overcharging, and discharging significantly impact the internal
47 electrochemical behaviour of LIBs and may cause potentially hazardous phenomena such as
48 thermal runaway (TR), which can lead to serious safety risks, including fire, explosion, or the
49 release of toxic gases^{4,5}. To reduce safety risks and economic losses, implementing early screening
50 and warning strategies is essential for abnormal faults in LIBs.

51 Current LIB safety detection strategies entail monitoring parameters such as strain, temperature,
52 gas concentration, and electrical characteristics⁶⁻⁹, playing crucial roles in detecting abnormal faults
53 at different stages of the LIB lifetime. However, thermocouples and voltage or current
54 measurements can only detect obvious battery failures when at least one cell is in a TR state.
55 Moreover, detecting a gas venting event that occurs prior to the TR state using thermocouples and
56 voltage measurements is challenging, because the working voltage remains stable, and the location

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57 of the temperature increase is usually unknown⁹. On the other hand, gas sensors can detect battery
58 failures approximately 7–8 min prior to TR by monitoring gas emission, enabling earlier detection
59 of battery failure compared to temperature, voltage, and current measurements^{10, 11}.

60 Trace amounts of electrolyte vapour leakage can be considered an early symptom of LIB damage⁹.
61 The electrolyte mixture used in LIBs typically contains volatile carbonate-based organic solvents
62 that can be detected using volatile organic compound (VOC) sensing technology, helping achieve
63 rapid and early warning of LIB failure at room temperature^{5, 12}. VOC detection by gas
64 chromatography-mass spectrometry has high sensitivity and selectivity in the parts per trillion range;
65 however, its application is constrained by complex calibration operations and the need for off-site
66 testing¹³. To overcome these limitations, alternative VOC sensing technologies have been proposed,
67 such as quartz crystal microbalances¹⁴, and electrochemical gas sensors¹⁵, thermal conductivity gas
68 sensors¹⁶, and metal oxide semiconductor gas sensors¹⁷. However, quartz-crystal microbalances are
69 not suitable for rapid detection despite their high sensitivity, electrochemical gas sensors are limited
70 by zero drift and aging, thermal conductivity gas sensors exhibit good operational stability but
71 suffer from low sensitivity and poor detection accuracy, and metal oxide semiconductor gas sensors
72 are easily influenced by environmental factors, such as high temperature and humidity. Overall, the
73 aforementioned techniques are limited by electromagnetic interference, extreme working
74 environments, and low sensitivity, rendering them unsuitable for in situ trace detection of VOCs
75 from LIBs.

76 In recent years, optical fibre sensors have emerged as promising candidates in the field of VOC
77 sensing due to minimal disturbance by environmental factors, and their compact size, high
78 sensitivity, and short response time. As a result, these advancements have garnered significant
79 attention and led to remarkable progress in the field^{18–21}. Among these, external interferometers,
80 such as the Mach-Zehnder interferometer (MZI), possess long interference arms that provide high
81 sensitivity; however, they require complex demodulation methods and devices, making them large
82 and expensive²². Moreover, the Fabry-Pérot interferometer is insensitive to the refractive index (RI)
83 of reflecting surfaces and is unstable due to changes in cavity length caused by various
84 disturbances²³. Various specialty optical fibres sense changes in RI induced by the interaction of
85 light with matter. However, the vast majority do not generate a sufficiently strong evanescent field²⁴,
86 ²⁵, which limits sensitivity. Notably, MNF have a waist region diameter on the micro/nano scale,
87 making them compact and facilitating both the coupling of external disturbances into the ultra-high

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88 evanescent field and the decoupling of disturbances through wavelength or intensity demodulation
89 methods. Compared with other optical sensors, MNFs can detect the RI of the external environment
90 with ultrahigh sensitivity owing to their high evanescent field^{22, 26–28}. In summary, considering the
91 need for simple demodulation methods, high sensitivity, and low disturbance requirements for VOC
92 sensing, MNFs are the most appropriate choice.

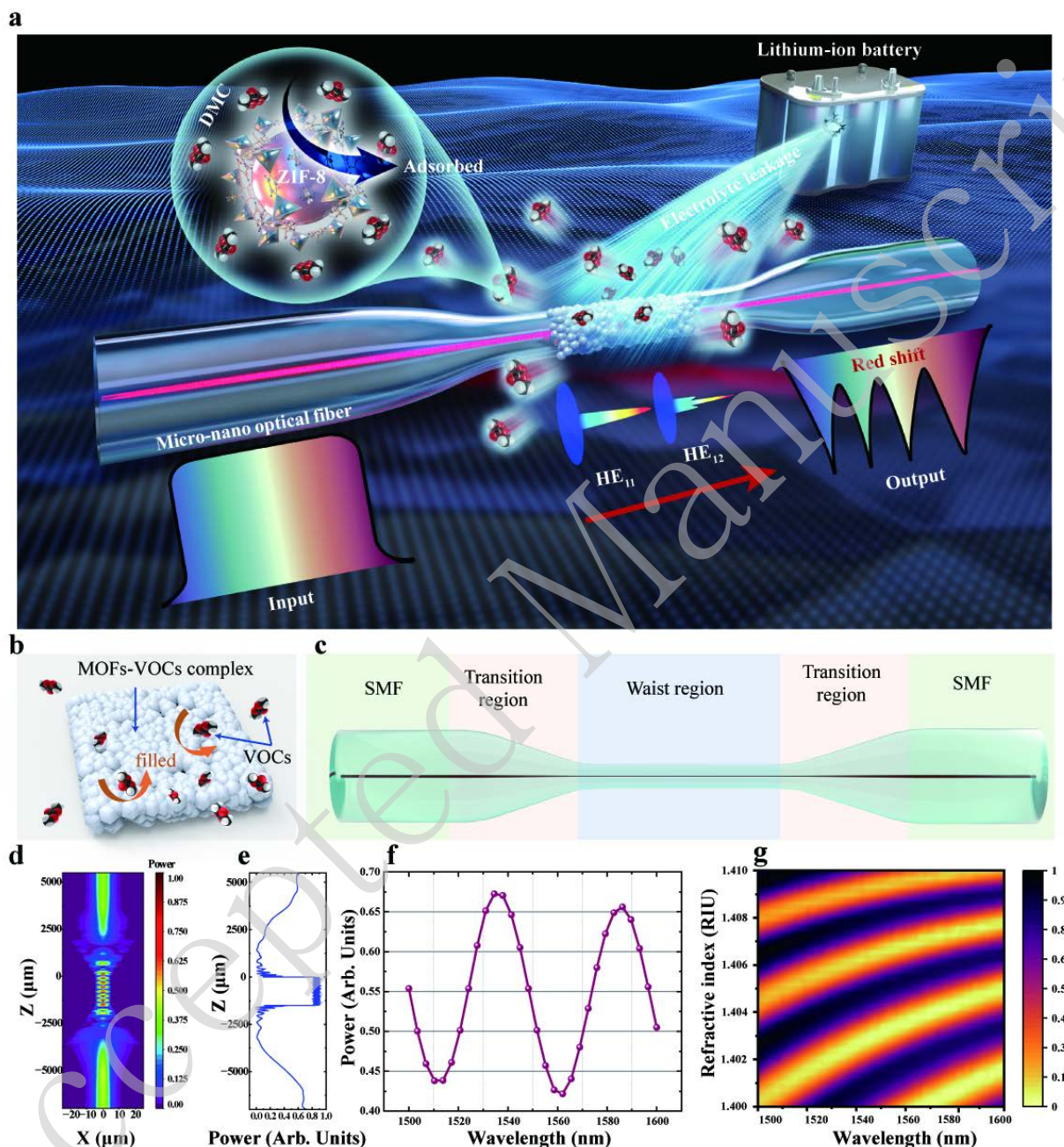
93 Despite their advantages, detecting trace amounts of VOCs poses a challenge for MNFs due to
94 the weak modulation of the RI of air near the surface of the VOC sensor at ppm concentrations.
95 Hence, VOC adsorbent materials are necessary as gas-sensitive layers to increase the VOC
96 concentration on the sensor surface by several orders of magnitude. Typically, MNFs are
97 functionalized to enhance their ability to detect specific substances. However, functionalized
98 materials rely on weak van der Waals forces to interact with MNFs, which renders the materials on
99 the fibre unstable owing to their small surface area and thickness. This instability leads to an
100 uncontrollable and unpredictable final optical spectrum, making them unsuitable for stable
101 measurements of LIBs^{29, 30}. Improving functionalization methods is necessary to enhance gas
102 detection sensitivity. To date, a range of VOC sensitive materials have been reported, such as
103 organic polymers³¹, carbon nanotubes³², zeolites³³, metal oxides³⁴, and metal–organic frameworks
104 (MOFs)³⁵. Among these materials, zeolitic imidazolate framework-8 (ZIF-8) exhibits exceptional
105 adsorptivity for VOC gas molecules due to its porous properties. Furthermore, ZIF-8 can
106 functionalize MNFs via in situ self-assembly through the formation of strong chemical bonds. Thus,
107 ZIF-8 is a promising candidate for VOC adsorption and offers a potential solution for increasing the
108 effective RI of the sensitive surface layer of MNFs³⁶.

109 In this study, a high-sensitivity LIB sensor has been proposed and demonstrated to warn LIB
110 faults at an early stage of electrolyte leakage through VOC sensing. The sensor utilizes MNFs as the
111 substrate, onto which a controlled, in situ self-assembled ZIF-8 membrane was deployed as the
112 sensitive layer; the proposed sensor is referred to as MNFs*ZIF. The performance of MNFs *ZIF
113 under various concentrations of LIB electrolyte components was measured and calibrated with high
114 sensitivity and fast response time through wavelength demodulation. In addition, MNFs*ZIF was
115 employed for online leakage monitoring of LIBs under working conditions for the first time,
116 providing early warning prior to the load ceasing. The proposed LIB sensor can provide high
117 sensitivity and stable detection of VOCs, as well as a fast response to LIB electrolyte leakage,

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118 illustrating its potential application in the early warning of faulty LIBs in various commercial
119 products, such as electric cars.

120 **Concept and methodology**



121 **Figure 1. Experimental concept and design principle.** LIB electrolyte vapour detection by MNFs*ZIF. **a**,
122 Concept of electrolyte detection in LIBs using ZIF-8 membrane-coated MNFs; small quantities of electrolyte
123 leaked from LIBs evaporates, generating gaseous DMC molecules, which causes a red-shift in the
124 transmission spectrum of DMC observed by MNFs*ZIF. **b**, Schematic of microporous MOFs filled with
125 VOCs to modulate the RI of the MOF-VOC complex. **c**, Typical structural diagram of MNFs, including
126 G.652 SMF, with the transition region featuring a steep taper assigned to the exciting HE_{12} mode, and the
127 waist region, several micrometers in diameter, where interference between HE_{12} and HE_{11} occurs. **d**, Intensity

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129 contour map of light propagation along MNFs*ZIF, simulated using Rsoft, where the fundamental mode is
 130 set as the launch light field, the monitored path represents the fibre core, and the output observing target
 131 corresponds to the fibre base mode power in MNFs*ZIF, with the MNF modelled as an exponentially shaped
 132 transition region. Light is confined to the fibre core in the SMF region, resulting in leakage of light power
 133 into the cladding of the transition region. The modes of interference generate high-frequency power
 134 oscillations in the waist region. **e**, Normalized power curve of the HE₁₁ mode along the light propagation axis
 135 of MNFs*ZIF under the fundamental mode light field input. **f**, Simulated transmission spectrum of
 136 MNFs*ZIF from 1500 to 1600 nm with a wavelength sampling point of 30. **g**, Intensity contour map of the
 137 MNFs*ZIF transmission spectrum from 1400 to 1600 nm with a wavelength sampling point of 60, and the
 138 cladding RI ranging from 1.40–1.41 with a RI sampling point of 30.

139 The schematic diagram of the LIB leakage and ZIF-8 adsorption processes is shown in Fig. 1a.
 140 The MNFs*ZIF was suspended on a bracket at the top of the chamber, together with the LIB cell
 141 located at the bottom. Input and output optical signals were transmitted through single-mode optical
 142 fibre (SMF) patch cords and flanges on the chamber. When the LIB fails, traces of electrolyte leak
 143 and quickly evaporate into VOCs. A typical electrolyte vapor is dimethyl carbonate (DMC) vapor,
 144 which migrates towards the top of the chamber and is adsorbed within the ZIF-8 pores. The MNFs,
 145 functioning as mode interference MZIs, are coated with an in situ self-assembled ZIF-8 membrane.
 146 Given its large specific surface area and high porosity, DMC can be adsorbed by the ZIF-8
 147 membrane, modulating the RI of the evanescent field in the MZI. DMC adsorption increases the
 148 external RI of the MNFs, resulting in a red-shift in the transmission spectrum. Conversely,
 149 desorption of VOCs induces a blue-shift, allowing for the determination of RI variation through
 150 wavelength demodulation.

151 For optical VOC sensors, determining how the volume fraction of the target analyte in the MOF
 152 film alters the effective RI of the MOF-VOC complex is crucial, as shown in Fig. 1b. This
 153 relationship can be described by the following general equation for the RI of microporous substrates
 154 filled with a fluid analyte³⁷:

$$n = \sqrt{(V_{sub}n_{sub}^2 + V_a n_a^2 + (1 - V_{sub} - V_a)n_{vac}^2)} \quad (1)$$

155 where V_{sub} and V_a represent the volume fractions of the microporous substrate and fluid analyte,
 156 respectively, and n_{sub} , n_a , n_{vac} , and n represent the RI indices of the microporous substrates, fluid
 157 analyte, vacuum, and substrate-analyte complex, respectively. Given that the effective RI of the
 158 ZIF-8 membrane without the analyte (n_{zif}) and filled with DMC vapour ($n_{dmc-zif}$) is known, the
 159 volume fraction of DMC vapour in the ZIF-8 substrates (V_{DMC}) can be expressed by a simplified
 160 equation:

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$$V_{DMC} = (n_{dmc-zif}^2 - n_{zif}^2) / (n_{dmc}^2 - n_{vac}^2) \quad (2)$$

161 According to this relationship, the volume fraction of DMC vapour in the ZIF-8 substrate
 162 increases as DMC vapour is adsorbed by the ZIF-8 membrane, which macroscopically manifests as
 163 an increase in the effective RI of the ZIF-8 membrane³⁷. A schematic of the MNF structure as
 164 sensing carriers for LIB monitoring is depicted in Fig. 1c. When the HE₁₁ fundamental mode in a
 165 SMF is transmitted to tapered MNFs, the higher-mode HE₁₂ is excited in the transition region and
 166 leaks into the cladding. Subsequently, mode coupling occurs between HE₁₁ and HE₁₂, allowing
 167 them to propagate together along the waist region until the energy is recoupled back into the SMF
 168 core through another symmetrical transition region, forming a mode interference MZI³⁸. Due to the
 169 dual-mode interference in MNFs, the wavelength demodulation method is utilised instead of
 170 intensity demodulation, effectively improving sensing accuracy and detection range while avoiding
 171 interference caused by light source fluctuations.

172 As the RI of the ZIF-8 membrane surrounding the MNFs changes, distinct changes in the
 173 effective RIs of the two modes occur, resulting in a shift in the transmission spectrum that can be
 174 demodulated using the wavelength demodulation method. The RI sensitivity of MNFs can be
 175 characterised by the following relationship:

$$S = d\lambda_N / dn = (\lambda_N \frac{\partial(\Delta n_{eff})}{\partial n_{SRI}}) / (\Delta n_{eff} - \lambda_N \frac{\partial(\Delta n_{eff})}{\partial \lambda_N}) \quad (3)$$

176 where $G = \Delta n_{eff} - \lambda_N (\partial(\Delta n_{eff}) / \partial \lambda_N)$ is the group effective RI difference between the HE₁₁ and
 177 HE₁₂ modes, representing the dispersion characteristics of the MNFs. Since the input wavelength is
 178 approximately 1550 nm, the impact of variation in λ can be neglected. Therefore, the RI sensitivity
 179 of MNFs is primarily determined by G , λ_N , and $\partial(\Delta n_{eff}) / \partial \lambda_N$ ³⁹.

180 To study the optical properties of the proposed MNFs*ZIF sensor, a simulation based on Rsoft
 181 was conducted. A MNF with waist diameter of 7 μ m was selected to balance sensitivity and
 182 robustness. The thickness of the ZIF-8 membrane was set to 500 nm to optimize sensitivity while
 183 minimizing extinction in the transmission spectrum. The RI of ZIF-8 was estimated to be 1.4,
 184 according to previous reports³⁹.

185 The simulation results are displayed in Fig. 1d–g. The intensity of light propagation through the
 186 MNF is shown in Fig. 1d, while Fig. 1e illustrates the optical power of the HE₁₁ mode monitored
 187 along the MNFs, revealing the power oscillation phenomenon caused by mode coupling in the waist

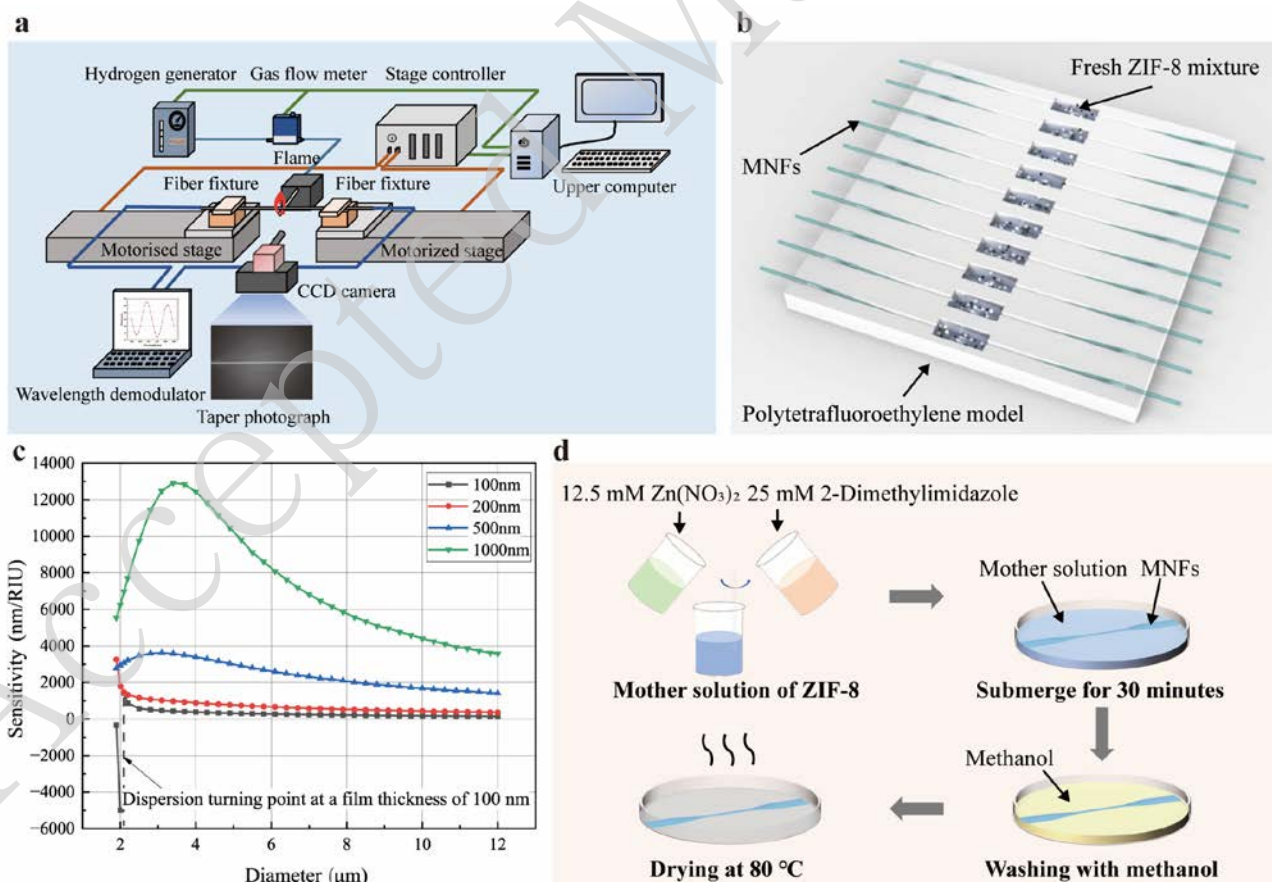
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188 region. To obtain the theoretical transmission spectrum, the input wavelength was scanned from
 189 1500 to 1600 nm, as shown in Fig. 1f. Assuming that the cladding material of the MNFs is ZIF-8
 190 and that the RI variation of the cladding ZIF-8 is +0.1 RIU due to the adsorption of DMC vapor, the
 191 results indicate a red-shift of several thousand nanometres, as depicted in Fig. 1g. This observation
 192 confirms that the MNFs*ZIF sensor has an RI sensitivity of 24166.3 nm/RIU when the MNF
 193 cladding material is a ZIF-8 membrane with a RI of 1.4. Therefore, the simulation results indicate
 194 that the MNFs*ZIF sensor possesses ultrahigh theoretical RI sensitivity, capable of meeting the
 195 requirements for detecting trace VOC concentrations.

196 Fabrication and experimental methods

197 Fabrication of MNFs*ZIF

198 MNFs were fabricated by rapidly drawing melted SMF using a hydrogen-oxygen flame. A
 199 schematic of the MNF fabrication system is depicted in Fig. 2a. An MNF with a uniform waist
 200 region diameter of 7 μm and a smooth surface was obtained using a hydrogen flow of 85 $\text{mL}\cdot\text{min}^{-1}$
 201 and a distance of 4.5 mm between both the motorized stages, with a drawing speed of 0.15 $\text{mm}\cdot\text{s}^{-1}$.



202
 203 **Figure 2. Methods for fabrication and ZIF-8 functionalization of the MNFs*ZIF sensor.** **a**, Schematic of
 204 the MNF fabrication system. This system employs a wavelength demodulator to select the required

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205 transmission spectrum, while a CCD camera ensures that the fiber remains aligned along the same axis
206 during the stretching process, facilitating real-time observation of the tapering process. **b**, Schematic of
207 ZIF-8 in-situ self-assembly on the MNFs within a polytetrafluoroethylene model. This model supports the
208 fabrication of up to 10 MNFs*ZIF from the same batch, with each solution container having a volume of 1.5
209 mL. The waist region of the MNFs is suspended and clamped in the model, where in-situ ZIF-8
210 self-assembly, cleaning with a methanol solution, and vacuum drying are performed to ensure the stability of
211 the adhered ZIF-8 on the MNF. **c**, Relationship between sensitivity, film thickness, and diameter; the selected
212 parameters for the MNFs*ZIF include a 7 μm diameter MNF modified with a 500 nm thick ZIF-8 film,
213 based on a comprehensive analysis of sensitivity enhancement and sensor robustness. **d**, Depiction of one in
214 situ ZIF-8 self-assembly cycle on the MNF substrate at room temperature; each step is conducted within the
215 model without transferring the MNFs, and the mother solution is mixed in a 1:1 volume ratio, with equal
216 amounts injected into each model container.

217 To enhance the sensitivity of the MNFs to DMC vapor, an in situ self-assembled ZIF-8
218 membrane was coated onto the MNFs. ZIF-8 offers several advantages, including high stability,
219 hydrophobicity, a highly regular pore structure, adjustable pore and cage sizes, and variable
220 flexibility. The specific parameters deployed included a pore size of 3.4 nm, cage diameter of 11.6
221 nm, specific surface area of $1730 \text{ m}^2 \cdot \text{g}^{-1}$, and pore volume of $0.63 \text{ m}^3 \cdot \text{g}^{-1}$. The materials used in this
222 process included zinc nitrate hexahydrate, 2-methylimidazole, methanol, and dimethyl carbonate,
223 all of which were of analytical purity and used without further purification. Given that the waist
224 diameter and evanescent field depth of the dual-mode interference MNFs were in the micrometer
225 range, the thickness of the ZIF-8 film was preferably set to the micrometer range or below. This
226 ensured efficient coupling between the change in RI of the ZIF-8 film and the evanescent field of
227 the MNFs, while also supporting stable growth of the film on the MNFs substrate. The in situ
228 self-assembly environment is illustrated in Fig. 2b, where the MNFs were fixed in the groove of a
229 polytetrafluoroethylene model, keeping them straight and suspended to ensure that the waist region
230 of the MNFs could be fully immersed in the central compartments for in situ self-assembly.

231 To analyse the optimised quantity and thickness of ZIF-8, a simulation was conducted using
232 Comsol, setting the RI of ZIF-8 at 1.4. The MNF RI sensitivity was modified using ZIF-8 films
233 with thicknesses of 100 nm, 200 nm, 500 nm, and 1 μm . As illustrated in Fig. 2c, although reducing
234 the diameter of the MNFs can improve sensitivity, the diameter should not be too small to ensure
235 the robustness of the sensor and fabrication success rate. In addition, a thicker ZIF-8 film resulted in
236 increased responsiveness of the sensor but led to greater loss of the HE_{12} mode, decreasing the
237 extinction ratio of the transmission spectrum. Therefore, after considering factors such as robustness,
238 sensitivity, accuracy, and fabrication success rate, the optimal configuration was determined to be a

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239 500 nm-thick ZIF-8 film modified onto 7 μm diameter MNFs, achieving a sufficiently high RI
240 sensitivity of 2326 nm/RIU.

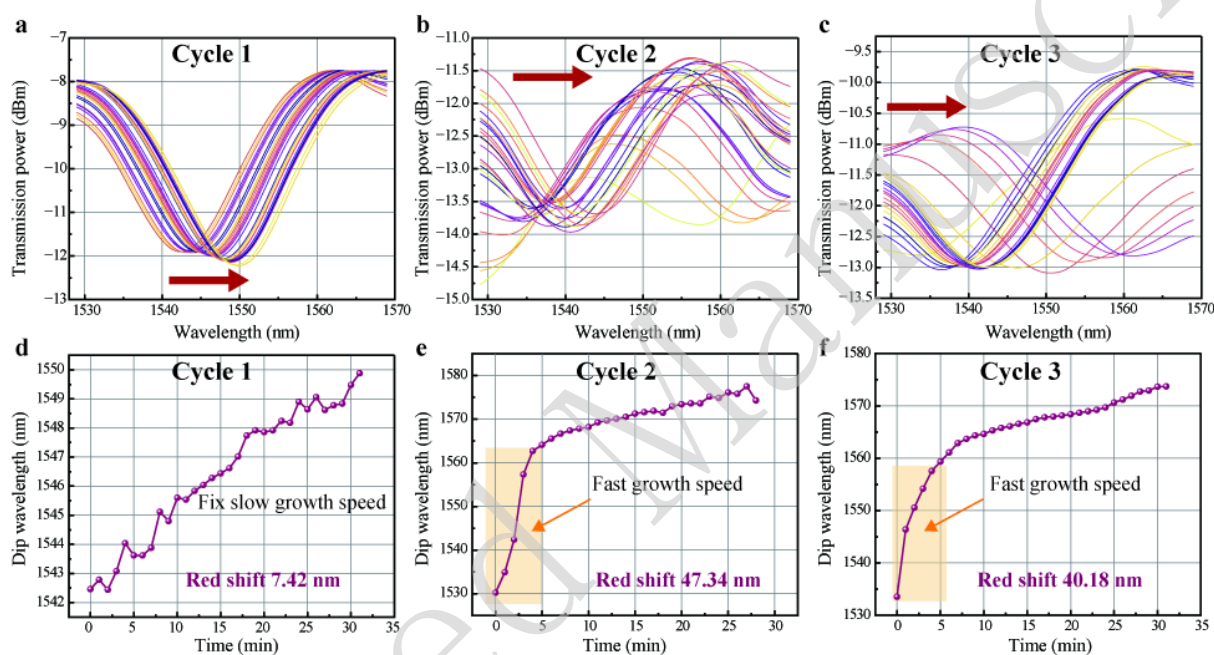
241 ZIF-8 films were grown in situ on the surface of MNFs through intermolecular hydrogen bonding
242 interactions, affording stable gas-sensing materials. By optimising the crystallisation process, dense
243 and highly crystalline ZIF-8 thin films were successfully generated on the MNFs. The in situ ZIF-8
244 self-assembly process is illustrated in Fig. 2d and can be described through the following steps:
245 First, a 20 mL methanol solution containing 12.5 mM zinc nitrate hexahydrate was mixed with
246 another 20 mL methanol solution containing 25 mM 2-methylimidazole and stirred at room
247 temperature. The freshly prepared mixture was then transferred to containers, and the MNFs were
248 submerged in the solution. After 30 min, the MNFs were thoroughly washed thrice with methanol
249 and dried. This sequence of steps constitutes one in situ self-assembly cycle. Following four cycles
250 of this process, the modified MNFs were dried in a vacuum oven at 80 $^{\circ}\text{C}$ overnight to yield the
251 LIB sensor⁴⁰. Due to the columnar molecular structure of ZIF-8, the material exhibits a greater
252 capacity for adsorption compared to similar chain molecules⁴¹, indicating that the van der Waals
253 forces between the VOCs from batteries and ZIF-8, along with the hydrogen bond acceptors
254 capable of generating strong hydrogen bonds with ZIF-8, are relatively strong. However, cyclic gas
255 molecules such as toluene face challenges in entering the ZIF-8 pores because of their larger
256 molecular cross-sectional area. Smaller molecules, such as hydrogen, present a minor difference in
257 RI compared to air, resulting in a low response in wavelength shift. In addition, non-polar
258 molecules in the atmosphere, such as nitrogen and oxygen, lack entities capable of hydrogen
259 bonding, leading to only weak interactions with ZIF-8. Consequently, sensors designed with this
260 material demonstrate excellent selectivity and are largely immune to interference from other volatile
261 compounds, including hydrogen, toluene, and nitrogen.

262 **Monitoring in situ self-assembly**

263 To further analyse the in situ self-assembled ZIF-8 membrane on the MNFs and verify the
264 effective crystallisation in the waist region of the MNFs, the evolution of the transmission spectrum
265 during the first three crystallisation cycles was monitored, as illustrated in Fig. 3. The results
266 indicate that the extinction ratio of the transmission spectrum of MNFs decreases with an increasing
267 number of crystallisation cycles, as shown in Fig. 3a–c. This decrease is attributed to the increase in
268 optical loss of the HE_{12} mode, which occurs with the increasing thickness of the ZIF-8 membrane,
269 leading to a greater power difference between the HE_{11} and HE_{12} modes. Additionally, the data

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270 reveal that the first crystallization cycle induced only a minor red-shift of 7.42 nm in the
 271 transmission spectrum. In contrast, the second and third growth cycles resulted in significant
 272 red-shifts of 47.34 nm and 40.18 nm, respectively, as depicted in Fig. 3d–e. These observations
 273 suggest that ZIF-8 underwent nucleation during the first crystallization cycle, forming a seed layer
 274 characterized by a slow growth rate. In subsequent cycles, particularly during the second and third
 275 cycles, the growth process accelerated, especially within the first 5 min. This monitoring of the
 276 transmission spectrum provides valuable information regarding crystal growth, thereby facilitating
 277 the controlled manufacturing of MNFs*ZIF sensors.



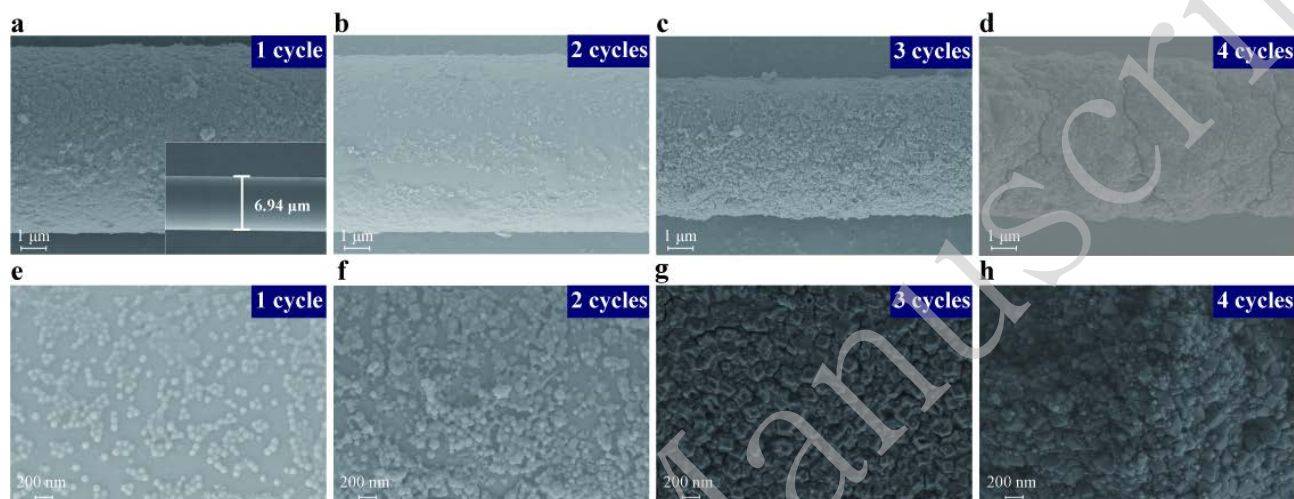
278
 279 **Figure 3. In situ self-assembly process for ZIF-8 monitored by the transmission spectra of the MNFs**
 280 **during the first three growth cycles.** The ZIF-8 was self-assembled in situ on the surface of bare MNFs
 281 layer by layer, with the transmission spectrum of the MNFs at a frequency of 1 min over approximately 30
 282 min. **a**, Evolution of the red-shift in the transmission spectrum recorded during the first growth cycle,
 283 with measurements taken after 32 min. **b**, Evolution of the red-shift in the transmission spectrum recorded
 284 during the second growth cycle, with measurements taken after 29 min. **c**, Evolution of the red-shift in the
 285 transmission spectrum recorded during the third growth cycle, with measurements taken after 32 min. **d**,
 286 Curve of dip wavelength position during the first cycle of ZIF-8 growth, tracking the dip observed at
 287 approximately 1542 nm. **e**, Curve of peak wavelength position during the second cycle of ZIF-8 growth,
 288 tracking the dip at approximately 1530 nm. **f**, Curve of peak wavelength position during the third cycle of
 289 ZIF-8 growth, tracking the dip at approximately 1532 nm.

290 Morphological characterization

291 To analyse the crystallisation conditions for ZIF-8 on the surface of the MNFs, the ZIF-8
 292 membranes were morphologically characterised before and after 1–4 cycles of in situ self-assembly,
 293 as depicted in Fig. 4. The waist region diameter of the bare MNFs was approximately 7 μm ,

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294 exhibiting a smooth and uniform surface, as shown in the inset of Fig. 4a. Moreover, the size of the
 295 ZIF-8 crystals increased with the number of self-assembly cycles, resulting in a denser and more
 296 uniform ZIF-8 membrane. After four cycles of in situ self-assembly on bare MNFs, a ZIF-8
 297 membrane with a thickness of 506 nm was achieved, as illustrated in Fig. S2, which aligns with the
 298 simulated value of ZIF-8 membrane thickness. Collectively, the SEM images show that ZIF-8
 299 crystals were grown with regular particle morphologies, resulting in tight and thick membranes.



300

301 **Figure 4. SEM images of ZIF-8 membranes on MNFs following 1–4 self-assembly growth cycles.** The
 302 SEM images were obtained at 3 kV extra high tension. **a**, SEM image after 1 cycle of in situ ZIF-8
 303 membrane self-assembly on MNFs with a magnification of 9 k; the inset shows the SEM image of bare MNF
 304 with a diameter of 6.94 μm . **b–d**, SEM images of MNFs after 1 to 4 cycles of in situ ZIF-8 membrane
 305 self-assembly, all with a magnification of 9 k. **e–h**, Higher magnification SEM images of in situ ZIF-8
 306 membranes self-assembled on MNFs: **e**, 1 cycle at 30,000 \times , **f**, 2 cycles at 20,000 \times , **g**, 3 cycles at 30,000 \times ,
 307 and **h**, 4 cycles at 30,000 \times .

308 Experimental setup

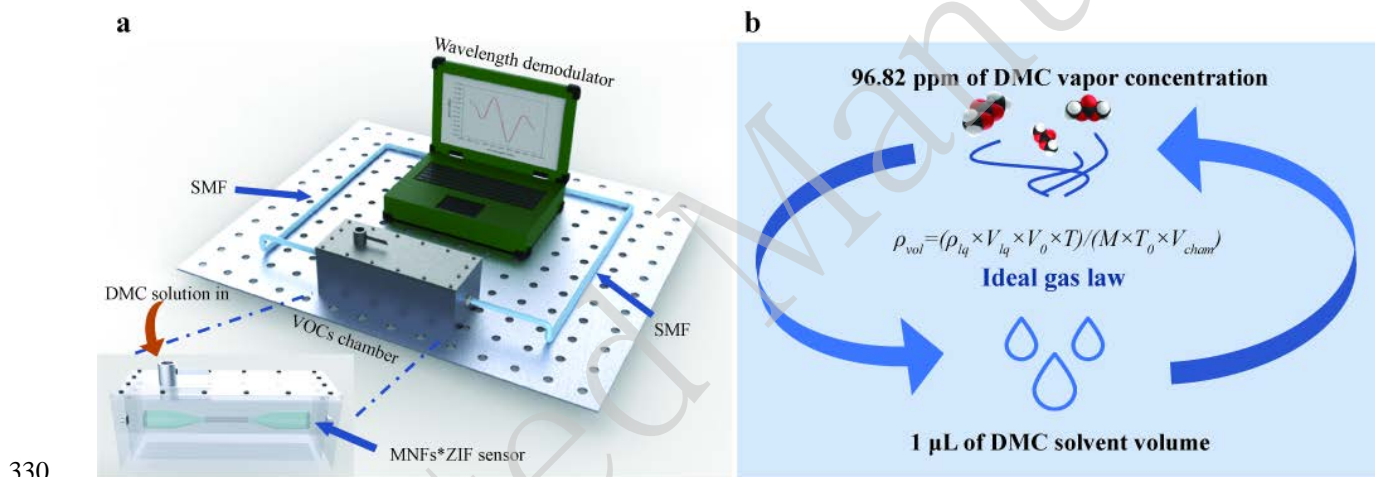
309 A schematic diagram of the wavelength demodulation sensing system for LIB electrolyte vapour
 310 detection is shown in Fig. 5a. The system primarily consisted of a gas chamber, wavelength
 311 demodulator, and fibre optic link. The fabricated MNFs*ZIF sensor was placed within a sealed
 312 metal gas chamber with a 3 L volume (100 mm \times 100 mm \times 300 mm), equipped with a spherical
 313 valve at the top for liquid introduction. The sensor was linked to a wavelength demodulator via two
 314 SMF patch cords to acquire and monitor the transmission spectrum. The wavelength demodulator
 315 recorded the transmission spectrum at intervals of 1 s or 1 min, over an acquisition range of 1530–
 316 1570 nm in the C-band. A 10 μL pipette gun was used to inject DMC solvent into the chamber,
 317 allowing the vaporized gas molecules to diffuse into the ZIF-8 membrane. The shift in the dip of
 318 specific interference patterns within the transmission spectrum was tracked to quantify the
 319 concentration of evaporated DMC.

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320 Since the target analyte was injected as a liquid, the gas concentrations after evaporation required
 321 conversion. According to the ideal gas law, under the conditions of 25 °C and standard atmospheric
 322 pressure, the conversion between the volume of DMC solvent (V_{liq}) and volume concentration of
 323 vapor (ρ_{vol}) in the gas chamber can be expressed as:

$$324 \quad \rho_{vol} = \left(\rho_{liq} \times V_{liq} \times V_0 \times T \right) / \left(M \times T_0 \times V_{cham} \right) \quad (4)$$

325 Here $\rho_{liq} = 1.07 \text{ g} \cdot \text{cm}^{-3}$ represents the DMC solvent density, $V_0 = 22.4 \text{ L} \cdot \text{mol}^{-1}$ is the standard
 326 molar volume of gas, $T_0 = 273 \text{ K}$ ($T = 298 \text{ K}$) is the temperature, $M = 90.078 \text{ g} \cdot \text{mol}^{-1}$
 327 represents the molar mass of DMC, and $V_{cham} = 3 \text{ L}$ is the volume of the chamber. Using this
 328 relationship, the volume fraction of DMC vapor after the complete evaporation of 1 μL of the DMC
 329 solvent in the gas chamber was calculated to be 96.82 ppm, as shown in Fig. 5b.



330
 331 **Figure 5. Experimental setup for detecting LIB electrolyte vapor concentration.** **a**, Schematic diagram
 332 of the MNFs*ZIF wavelength demodulation system, including the MNFs*ZIF sensor, VOC detection
 333 chamber, wavelength demodulator, and SMF patch cables. The wavelength demodulator featured an
 334 integrated light source, Bragg grating, photo detector, acquisition card, upper computer, and signal
 335 processing algorithms. The MNFs*ZIF sensor was positioned at the top of the gas chamber to ensure
 336 complete adsorption of evaporated solvent molecules. Silicone-sealed holes maintained the chamber's
 337 airtightness, and a ball valve at the top allowed for rapid electrolyte injection. **b**, Schematic illustrating the
 338 conversion between volume of the LIB electrolyte solvent and the resulting vapor concentration.

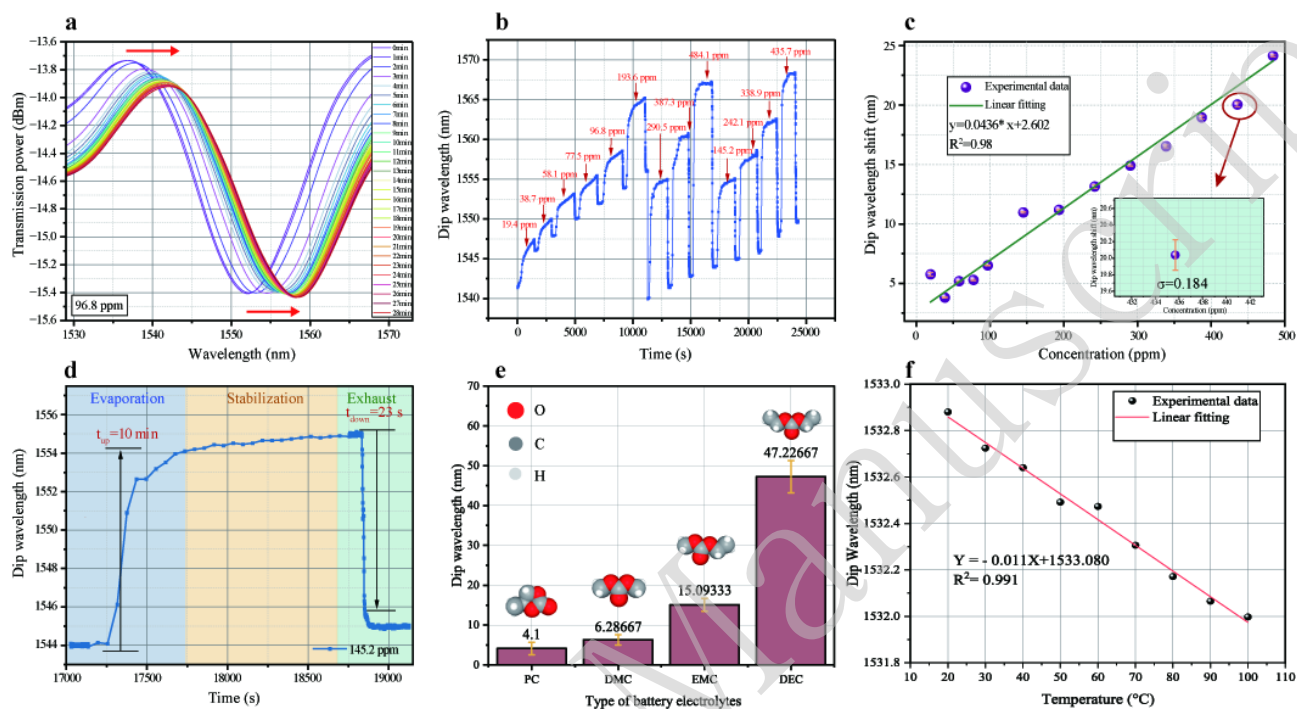
339 Results and discussion

340 Sensing performance for electrolyte vapor

341 To measure and calibrate the performance of the MNFs*ZIF sensor in detecting LIB electrolyte
 342 vapor, DMC, the most common electrolyte solvent in batteries, was chosen as the test analyte.
 343 Sequential injections of DMC solution (ranging from 0.2 to 4.5 μL) were administered into the gas

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344 chamber using a pipette gun. These volumes corresponded to vapor concentrations between 19.4
 345 and 435.7 ppm after full evaporation. The detection process was segmented into three phases:
 346 evaporation, stabilization, and exhaust, during which the transmission spectrum of the sensor was
 347 recorded at regular intervals. The detection outcomes are presented in Fig. 6.



348 **Figure 6. Performance of MNFs*ZIF in detecting LIB electrolyte vapor.** **a**, Evolution of the red-shift in
 349 the transmission spectrum of MNFs*ZIF over 28 min for a DMC vapor concentration of 96.8. **b**, Changes in
 350 the dip wavelength position in the transmission spectrum across time for DMC concentrations ranging from
 351 19.4 to 435.7 ppm, showing 13 distinct concentrations. The sensor's response phases include evaporation,
 352 stabilization, and exhaust. **c**, Linear fit of MNFs*ZIF sensor response to DMC concentrations between 19.4
 353 to 435.7 ppm, with error bars representing the standard deviation between pre- and post-adsorption
 354 stabilization phases. **d**, Example of response and recovery time for the MNFs*ZIF sensor to DMC vapor at
 355 145.2 ppm concentration. **e**, Resonant wavelength responses of MNFs*ZIF under 1 μ L volumes of various
 356 electrolyte compositions, including PC, DMC, EMC, and DEC, along with their chemical structures. **f**,
 357 Temperature sensitivity of MNFs*ZIF measured over a range of 20–100 $^{\circ}$ C in 10 $^{\circ}$ C/3-5min increments,
 358 controlled by a thermoelectric cooler.
 359

360 The transmission spectrum varied with DMC evaporation time, showing a typical red-shift as the
 361 evaporated DMC concentration increased from 19.4 to 193.6 ppm (Fig. 6a). In Fig. 6b, the
 362 interference dip wavelength consistently shifted to longer wavelengths, indicating good reversibility
 363 of the MNFs*ZIF sensor. After the sensor returned to its initial state, DMC concentration was
 364 incrementally raised from 290.46 to 484.1 ppm, maintaining consistent sensor reversibility.
 365 Repeated measurements at four concentrations (145.2 to 435.7 ppm) demonstrated repeatable
 366 sensor behavior. Notably, a slight red-shift during the stable period followed each test cycle due to
 367 minor instability in the wavelength demodulator's light source, which could be mitigated using

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368 signal processing techniques like wavelet denoising. The sensor's functionality was restored after
369 each cycle by air exchange to remove residual gas molecules on the ZIF-8 surface. Linear fitting
370 yielded a sensitivity S of 43.6 pm/ppm for the 19.4–435.7 ppm range, with $R^2 = 0.98$ (Fig. 6c), with
371 accuracy influenced by pipette volume precision.

372 Key performance metrics for VOC detection include response time (t_{up}) and recovery time (t_{down}),
373 defined as the time to reach 90% of the maximum wavelength shift during evaporation and exhaust
374 phases, respectively. t_{up} depended on complete evaporation and diffusion of DMC into ZIF-8, while
375 t_{down} depended on desorption rate, yielding $t_{up} = 10$ min and $t_{down} = 23$ s at 145.2 ppm (Fig. 6d).
376 Notably, the response time of the MNFs*ZIF sensor was influenced by the relatively slow processes
377 of electrolyte evaporation and penetration into the membrane pores. Recovery, however, was rapid
378 due to the passive venting process, where DMC vapor exchanged directly with the atmosphere.
379 Active venting, such as nitrogen injection, was not used. The significant concentration gradient
380 facilitated swift DMC-air exchange, reducing the RI and causing a spectral blue-shift. The standard
381 deviation of noise during a 120 s stable state without the target material was denoted as σ , with a
382 typical value of 0.0385 nm. Moreover, the limit of detection (LOD) for the MNFs*ZIF sensor was
383 defined as $3\sigma/S$, leading to a theoretical LOD of 2.65 ppm at a DMC concentration of 145.2 ppm.
384 With the wavelength demodulator resolution R set at 0.02 nm, the sensor's theoretical resolution R/S
385 was calculated to be 0.46 ppm, demonstrating the high sensitivity and low detection threshold of the
386 MNFsZIF sensor for DMC vapor.

387 To confirm the adsorption capabilities of MNFs*ZIF for LIB electrolytes, sensor responses to
388 four types of common electrolyte compositions was evaluated and compared, as shown in Fig. 6e.
389 Results indicated that the sensor was significantly more sensitive to diethyl carbonate (DEC) and
390 ethyl methyl carbonate (EMC) than to DMC and propylene carbonate (PC). The reduced response
391 to PC was attributed to its lower volatility relative to the other VOCs. Non-interference from other
392 volatiles, such as hydrogen, toluene, and oxygen, was confirmed based on the molecular adsorption
393 characteristics, including force, size, and polarity, analyzed during sensor fabrication. This selective
394 detection underscores the sensor's effectiveness, with the highest response observed for DEC. The
395 sensor's higher sensitivity to composite LIB electrolytes compared to single electrolytes like DMC
396 highlights its suitability for safety monitoring in battery leakage scenarios. Figure 6f illustrates the
397 sensor's temperature sensitivity, showing a minimal shift of -0.011 nm \cdot °C $^{-1}$ over the 20–100 °C
398 range, which is negligible for gas detection applications.

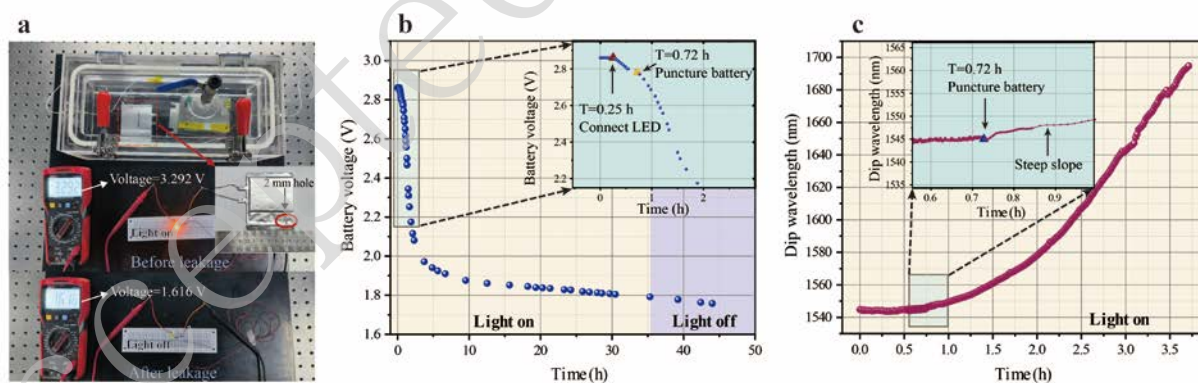
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399 In summary, the MNFs*ZIF sensor demonstrated exceptional sensitivity and resolution, with a
400 low detection limit and rapid response and recovery times for DMC vapor at ppm levels.
401 Performance comparisons with other VOCs sensor (Table S1) further emphasized its potential in
402 LIB leakage detection applications.

403 Online LIB leakage monitoring

404 To verify the capability of MNFs*ZIF for providing real-time early warnings of LIB leakage, an
405 experimental setup was created to simulate leakage from pouch lithium cells under working
406 conditions. The detection performance of MNFs*ZIF was compared to that of a light emitting diode
407 (LED) load to assess its effectiveness in identifying faults in defective batteries. The sensor and
408 battery were enclosed in an air-sealed chamber to prevent interference from other gases.

409 A pouch LIB cell containing DMC : DEC : EMC = 1:1:1 (v/v) electrolyte was placed in the
410 chamber, alongside the MNFs*ZIF sensor, with the LIB voltage monitored using a multimeter (Fig.
411 7a). First, the battery was tested under load to ensure it was functioning properly, powering the
412 LEDs with an initial voltage of 3.292 V. After 1 h, the battery voltage had dropped to 2.861 V,
413 marking the start of the monitoring phase. The voltage then continued to decrease at a consistent
414 rate as the LED consumed power from the LIB, as shown in Fig. 7b. To simulate a leakage event, a
415 puncture approximately 2 mm in diameter was made in the battery after 0.72 hours of monitoring
416 (Fig. 7a). Notably, this damage did not alter the rate at which the voltage decreased (Fig. 7b).



417 **Figure 7. Online leakage detection using the MNFs*ZIF sensor.** **a**, Diagram of the LIB electrolyte leakage
418 test system, where the MNFs*ZIF sensor was positioned at a high horizontal location in the chamber, and the
419 LIB was placed at the chamber's base. A pouch lithium cell with a nominal voltage of 3.65 V was punctured
420 with a hole approximately 2 mm in diameter to simulate leakage. An LED circuit, including a 100 Ω resistor
421 in series, completed the setup. The LIB's external voltage was continuously measured using a multimeter to
422 compare the voltage and LED status before (LED on, voltage = 3.939 V) and after (LED off, voltage = 1.616
423 V) the leakage event. **b**, Time-based variation of the LIB external voltage: at $T < 0.25$ h, the LIB remained
424 open; at $T = 0.25$ h, the LED was connected; at $T = 0.72$ h, the LIB was punctured, starting the leakage; at
425

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= 35 h, the LED was turned off. **c**, Changes in the MNFs*ZIF transmission spectrum's dip wavelength over
427 the first 3.5 h, recorded at 1-min intervals by the wavelength modulator, until saturation.

428 In contrast, the dip wavelength in the transmission spectrum of MNFs*ZIF showed an immediate
429 response to the leakage, characterized by a sudden steep slope (Fig. 7c), demonstrating the sensor's
430 capability to detect battery leakage with rapid response time. The dip wavelength underwent a
431 consistent red-shift of several hundred nanometers until saturation was achieved after 3.5 h,
432 effectively monitoring LIB leakage. Notably, even when the LIB voltage decreased to 2 V after this
433 period, the LED remained illuminated. The LIB voltage continued to decrease, reaching 1.616 V
434 until the leakage event occurred after 35 hours, at which point the LED load appeared to be off, as
435 illustrated in Fig. 7a. Overall, these results indicate that the MNFs*ZIF sensor is effective for online
436 monitoring of trace amounts of LIB electrolyte leakage and can provide early warnings of fault
437 events due to its high sensitivity, stability, rapid response time, immunity to other gases, and
438 robustness against temperature fluctuations.

439 **Conclusions**

440 In summary, a highly sensitive VOC sensor featuring in situ self-assembled ZIF-8 membrane-coated
441 MNFs has been fabricated for the early warning of online electrolyte leakage in LIB cells for the
442 first time. In our work, the detection principles of RI sensitivity in MNFs and the relationship
443 between the RI of the ZIF-8 membrane and VOC concentration was theoretically analysed.
444 Moreover, the MNFs*ZIF sensor was fabricated with a dense 500 nm thick in situ self-assembled
445 ZIF-8 membrane, which was grown in a controlled manner. To verify the performance of the
446 proposed MNFs*ZIF, gas concentration sensing experiments of DMC were carried out to calibrate
447 sensitivity, response time, and detection limit; the sensor achieved a sensitivity of 43.6 pm/ppm in
448 the ppm range for DMC vapour, as well as rapid response and recovery times averaging at 10
449 minutes and 23 seconds, respectively. The sensor also exhibited outstanding adsorption properties
450 for common electrolyte compositions over of other gases such as hydrogen and toluene.
451 Furthermore, a working-state LIB was monitored online by MNFs*ZIF, providing a red-shift of
452 hundreds of nanometres in the transmission spectrum and 35 h of early warning prior to the LED
453 load lights being switched off, demonstrating the excellent early warning capability of the
454 MNFs*ZIF. This study provides a highly sensitive, reversible, and fast response strategy for
455 promising energy and health diagnostics, with potential applications in electric cars, using in-situ
456 self-assembled ZIF-8 membrane-coated MNF sensors.

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461 **Author contributions**

462 Q.S. conceived the project. S.S. and H.L. conceived the study and designed the experimental
463 protocols. S.S. and Y.Z. jointly performed the experiments. L. L. and H. L. guided the fabrication
464 process. X.K. and X.H. guided the characterisation process. S. S., Y. L., and W. X. conducted the
465 theoretical analyses. Z. L., L. Y., Z. Y., and Y. H. contributed to the discussion of the results. Q.S.
466 revised the manuscript accordingly.

467 **Conflict of interests**

468 The authors declare no competing interests.

469 †These authors contributed equally to this work.

470 **Data availability**

471 The data supporting the plots and other findings in this study are available from the corresponding
472 authors upon reasonable request.

473 **Supplementary information**

474 Supplementary Information accompanies the manuscript on the Light: Advanced Manufacturing
475 website (<https://www.light-am.com/index.htm>), and includes details of the transmission spectra of
476 the MNFs after four growth cycle modifications (Fig. S1); an SEM image of the purified ZIF-8
477 powder (Fig. S2a); the thickness of the ZIF-8 membrane on the MNFs, as shown by SEM (Fig.
478 S2b); a powder X-ray diffractogram of the ZIF-8 membrane on the MNFs (Fig. S2c); recyclability
479 tests following 15 cycles (Fig. S3a); Bland-Altman error analysis of the 15-cycle recyclability tests
480 (Fig. S3b); and a summary of VOC sensor performances over the last decade (Table. S1).

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